



September 1, 2021

Mr. Maurice Rudolph HYDRY Company, LLC 4314 Pablo Oaks Court Jacksonville, Florida 32224

> ECS Project No. 35:29020-A1 Client ID: 3524

Reference: Preliminary Report of Geotechnical Exploration **River Landing Lot 57** Nocatee, St. Johns County, Florida

Dear Mr. Rudolph:

ECS Florida, LLC (ECS) has completed the requested preliminary geotechnical exploration in general accordance with our Proposal No. 35:17711-GPR dated April 5, 2021. The exploration was performed to explore the general subsurface conditions within the proposed lot area and to provide preliminary recommendations for foundation support.

Additional field testing should be performed to formulate detailed foundation design and site preparation and earthwork construction recommendations prior to final design. Once more detailed information regarding the proposed structure is developed, we should be given the opportunity to review and develop a supplemental design-phase scope of services.

PROJECT INFORMATION

The general site location is shown on the Site Location Diagram (Figure 1). At the time of our exploration, the site was undeveloped, with ground surface cover consisting of brush and trees. Surface water was not observed near the planned building area at the time of our exploration.

You provided a copy of a site plan for the subject site. This plan indicates the boundary limits for the property and the existing roadways adjacent to the site. However, we note the location of the proposed structure(s) was not available to our office at the time of this report preparation.

The following information explains our assumptions of the planned development.

SUBJECT	DESIGN INFORMATION / ASSUMPTIONS							
# of Stories	3 stories above grade							
Usage	Residential							
Column Loads ⁽¹⁾	50 kips							
Wall Loads ⁽¹⁾	3 kips per linear foot (klf) maximum							
Floor Loads ⁽¹⁾	150 pounds per square foot (psf) maximum							
Fill and Cut Heights	Assumed a maximum of 3 feet of fill and only minor cuts, from existing site grades							

(1) If actual structural loads differ from these assumed loads ECS must be contacted immediately in order to revise building foundation recommendations and settlement calculations, as needed.

FIELD EXPLORATION

We performed a field exploration on July 28, 2021 and August 10, 2021. The approximate boring locations are indicated on the attached Field Exploration Diagram (Figure 2). Our personnel determined the boring locations using a handheld Global Positioning System (GPS) unit. The boring locations on the referenced Field Exploration Diagram should be considered accurate only to the degree implied by the method of measurement used.

We located and performed two Standard Penetration Test (SPT) borings, drilled to depths of approximately 25 feet below the existing ground surface, in general accordance with the methodology outlined in ASTM D 1586 and two auger borings, drilled to depths of approximately 10 feet below the existing ground surface in general accordance with the methodology outlined in ASTM D 1452 to explore the subsurface conditions within the lot area. Soil samples recovered during performance of the borings were visually classified in the field and representative portions of the samples were transported to our laboratory for further evaluation. Our exploration procedures are explained in greater detail in Appendix B including the insert titled Subsurface Exploration Procedures.

VISUAL CLASSIFICATION

Each sample was visually classified on the basis of texture and plasticity in accordance with ASTM D2488 Standard Practice for Description and Identification of Soils (Visual-Manual Procedures) and including USCS classification symbols, and ASTM D2487 Standard Practice for Classification for Engineering Purposes (Unified Soil Classification System (USCS)). After classification, the samples were grouped in the major zones noted on the boring logs in Appendix B. The group symbols for each soil type are indicated in parentheses along with the soil descriptions. The stratification lines between strata on the logs are approximate; in situ, the transitions may be gradual.

GENERAL SUBSURFACE CONDITIONS

A graphical presentation of the generalized subsurface conditions is presented on Figure 3. It should be understood that the soil conditions will vary between the boring locations and in areas of the site not explored during our visit. The following table summarizes the soil conditions encountered.

Typical De	pth (ft)	Stratum	Description
From	То		
Existing Ground Surface	0.5 – 1	N/A	Topsoil
0.5 – 1	4 - 8.5	I	Very Loose to Medium Dense SAND (SP), varying amount of shell, Moist to Wet
4 - 8.5	6 – 12	П	Very Loose to Medium Dense SILTY SAND (SM) and CLAYEY SAND (SC), Wet
6 -12	25	111	Medium Dense SAND (SP), Wet

As exceptions, Borings NA 87 encountered a layer of clayey soil with roots at depths between approximately 6.5 feet and 8.5 feet below existing grades and Boring NB 87 encountered a layer of clayey sand few organic fines between depths of 8.5 feet and 12 feet below existing grades. We do not consider these layers suitable to remain in place below proposed structures. A graphical presentation of the subsurface conditions is shown on the Generalized Subsurface Soil Profiles in Appendix A.

Groundwater was encountered at each boring location and recorded at the time of drilling at depths of varying between approximately 3.4 feet and 5 feet below the existing ground surface. We note that groundwater levels will fluctuate due to seasonal climatic variations, surface water runoff patterns, construction operations, and other interrelated factors. The groundwater depth at each boring location is noted on the Generalized Subsurface Profiles and on the Log of Boring records.

PRELIMINARY DESIGN RECOMMENDATIONS

Our geotechnical engineering evaluation of the site and subsurface conditions at the property, with respect to the planned construction and our recommendations for earthwork and foundation support, are based on (1) our site observations, (2) the field and laboratory test data obtained, (3) our understanding of the project information and structural conditions as presented in this report, and (4) our experience with similar soil and loading conditions.

Additional field testing should be performed to formulate detailed foundation design and site preparation and earthwork construction recommendations prior to final design. Also, the discovery of any site or subsurface conditions during construction that deviate from the data obtained during this geotechnical exploration should also be reported to us for our evaluation.

Based on the above preliminary evaluation of the site and subsurface conditions at the borings with respect to the anticipated construction, it appears the proposed structure can be constructed on a deep foundation system.

Deep Foundation Support

The organic-containing soils can be left in-place if the proposed structure (including the floor slabs) is supported by deep foundations. There are several types of deep foundations; however, based on our experience with similar projects and soil conditions, Auger Cast In-Place (ACIP) piles are applicable. ACIP piles are constructed by drilling into the subsurface material with a continuous flight auger which is pulled

upward (after achieving the required length) while cement grout is pumped under pressure through the auger. Based on our experience with similar soil conditions, we expect that a 14-inch ACIP bearing 20-feet below the existing grades may develop an axial capacity on the order of 10 tons.

REPORT LIMITATIONS

Our geotechnical exploration has been performed, our findings obtained, and our recommendations prepared, in accordance with generally accepted geotechnical engineering principles and practices. ECS is not responsible for any independent conclusions, interpretation, opinions, or recommendations made by others based on the data contained in this report. Additional field testing should be performed to formulate detailed foundation design and site preparation and earthwork construction recommendations prior to final design.

Respectfully Submitted, **ECS FLORIDA, LLC**

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long mousand Joey Proussard, P.E.

Joey Broussara, P.E. **Principal Engineer** Registered Florida No. 58233 JBroussard@ecslimited.com

APPENDICES

Appendix A – Drawings & Reports

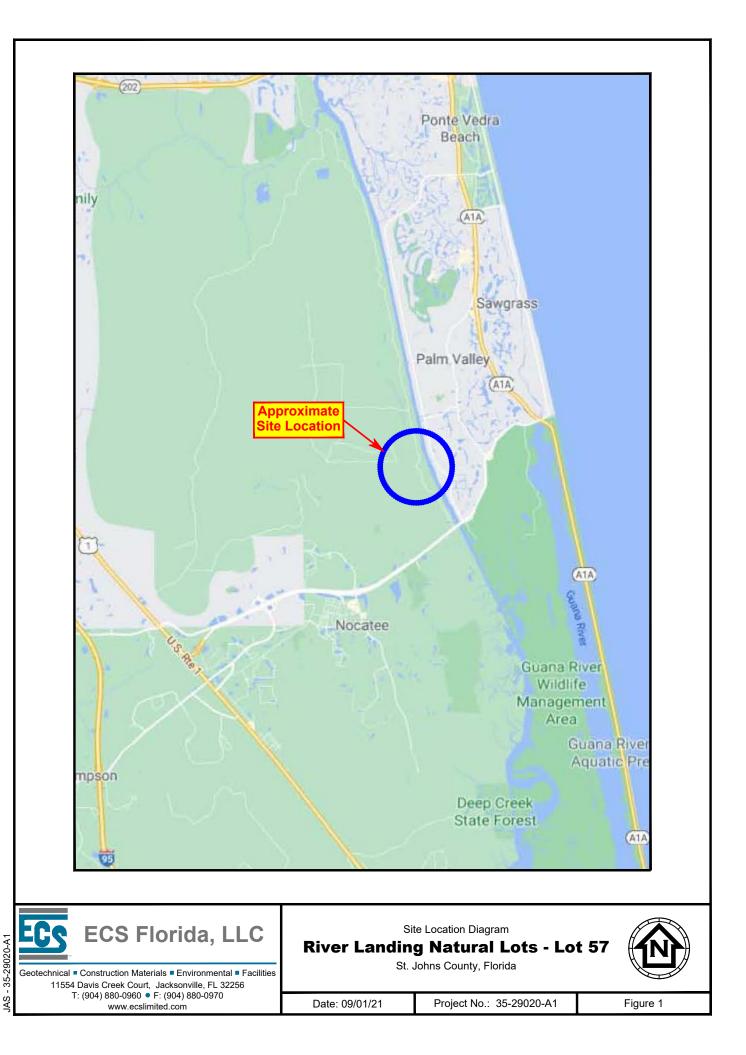
- Figure 1 Site Location Diagram
- Figure 2 Field Exploration Diagram
- Figure 3 Generalized Subsurface Profiles

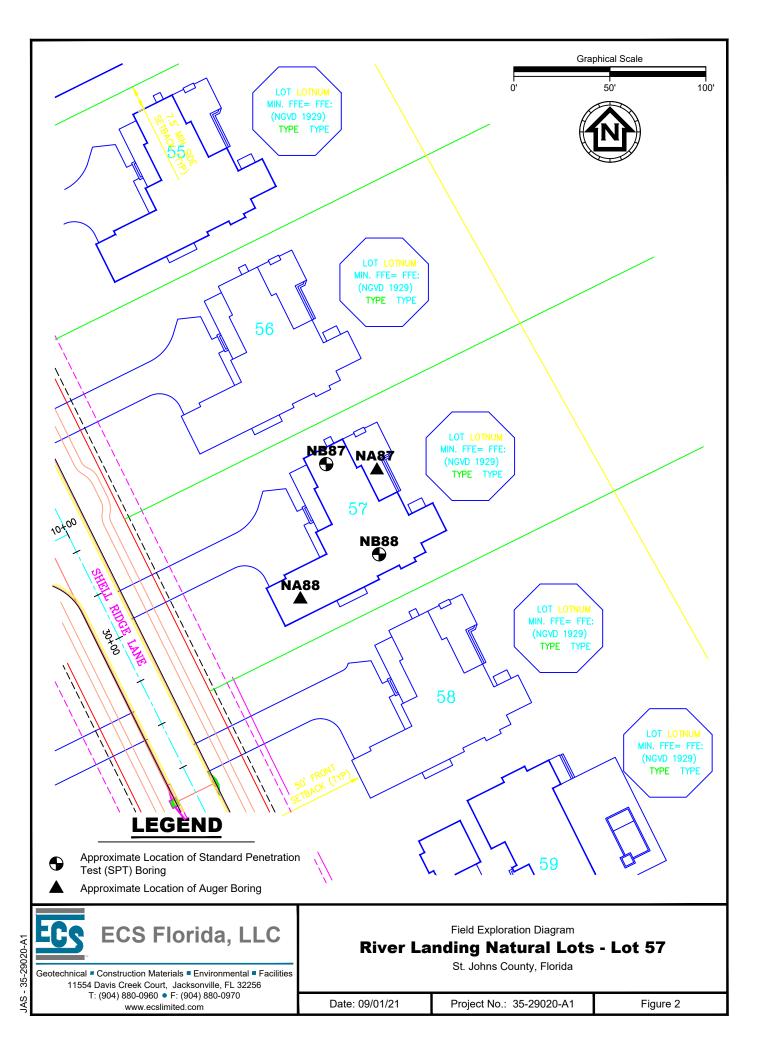
Appendix B – Field Operations

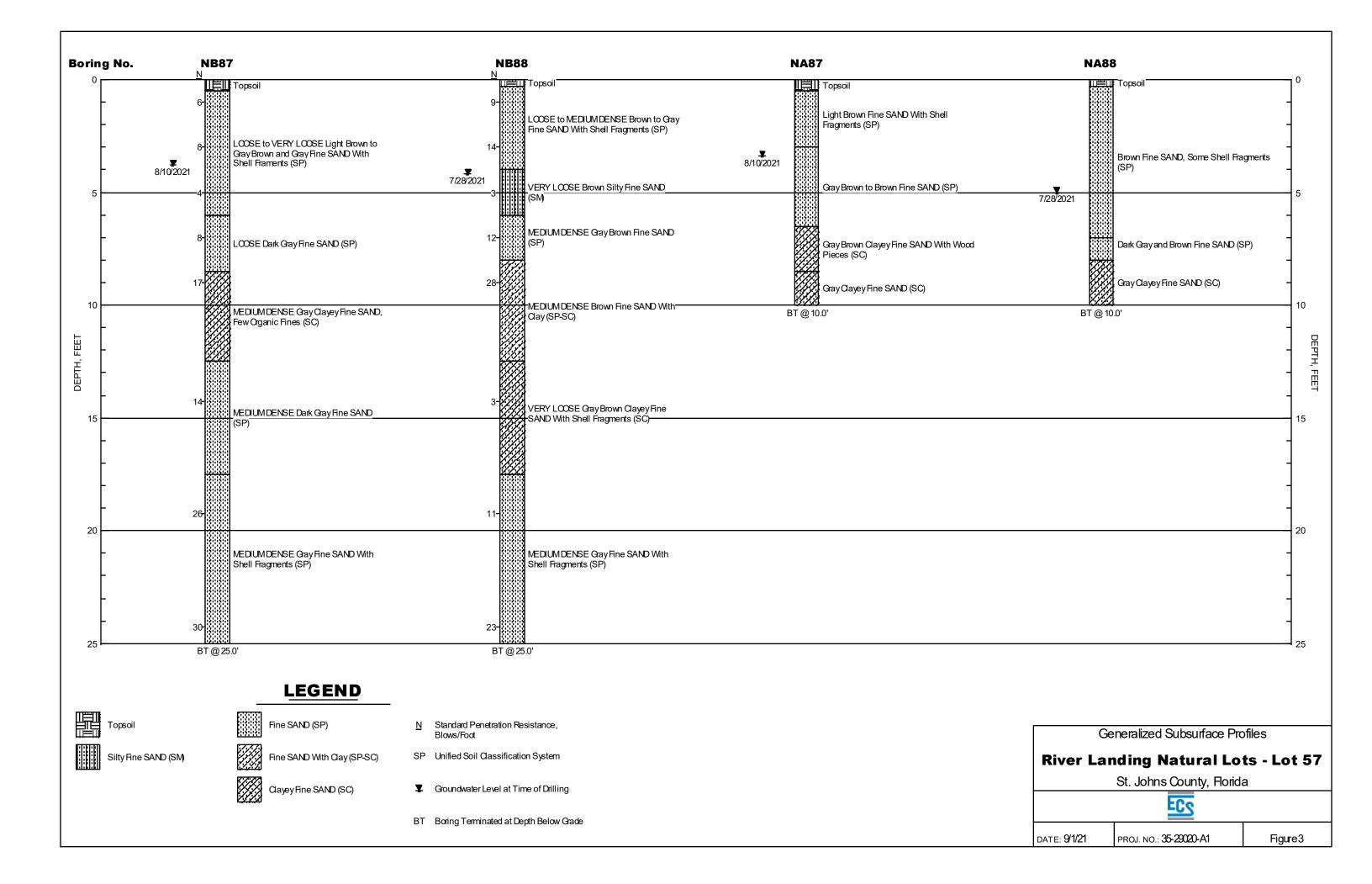
- Reference Notes for Boring Logs
- Subsurface Exploration Procedure: Standard Penetration Testing (SPT)
- Boring Logs

Appendix A – Drawings & Reports

Figure 1 - Site Location Diagram Figure 2 - Field Exploration Diagram Figure 3 – Generalized Subsurface Profiles







Appendix B – Field Operations

Reference Notes for Boring Logs Subsurface Exploration Procedure: Standard Penetration Testing (SPT) Boring Logs



REFERENCE NOTES FOR BORING LOGS

MATERIAL	1,2		DRILLING SAMPLING SYMBOLS & ABBREVIATIONS										
		HALT	SS	Split Spoor	n Sampler		PM						
	AJE		ST	Shelby Tub		RD	0						
	CON	CRETE	WS	Wash Sam	•	RC							
			BS	Bulk Samp		REC	, ,						
	GRA	VEL	PA	Power Aug	-	RQD	Rock Quality Designation %						
			HSA	Hollow Ste									
	TOP	SOIL	PARTICLE SIZE IDENTIFICATION										
	VOID		DESIGNA	TION	PARTI	CLE SIZES							
	VOIL		Boulder	S	12 i	inches (300 m	m) or la	rger					
	BRIC	ĸ	Cobbles	5	3 in	ches to 12 inc	hes (75	5 mm to 300 m	ım)				
			Gravel:	Coarse	3⁄4 ii	nch to 3 inches	s (19 mi	mm to 75 mm)					
	AGG	REGATE BASE COURSE		Fine	4.7	5 mm to 19 mr	m (No. 4	No. 4 sieve to ¾ inch)					
<u> </u>	GW		Sand:	Coarse	2.0	0 mm to 4.75 r	nm (No	. 10 to No. 4 s	sieve)				
-	GW WELL-GRADED GRAVEL gravel-sand mixtures, little or no fines			Medium	0.42	25 mm to 2.00	mm (N	o. 40 to No. 1	0 sieve)				
°°C	GP POORLY-GRADED GRAVEL			Fine		74 mm to 0.42	5 mm (l	No. 200 to No	. 40 sieve)				
ಿಂದ	0.	gravel-sand mixtures, little or no fines	Silt & C	lay ("Fines")	<0.	074 mm (smal	ler than	a No. 200 sie	eve)				
9°8	GM	SILTY GRAVEL	i				1		1				
64		gravel-sand-silt mixtures		COHESIVE	E SILTS &	CLAYS			COARSE				
18	GC	GC CLAYEY GRAVEL		NFINED				AMOUNT					
94		gravel-sand-clay mixtures		RESSIVE	SPT⁵	CONSISTENC	Y ⁷		(70)				
• •	SW	WELL-GRADED SAND		GTH, QP⁴	(BPF)	(COHESIVE	<u> </u>	Trace	<u><</u> 5				
• •		gravelly sand, little or no fines	1	0.25	<2	Very Soft		With	10 - 20				
	SP	POORLY-GRADED SAND gravelly sand, little or no fines	1	- <0.50	3 - 4	Soft							
	SM	SILTY SAND	1	- <1.00	5 - 8 9 - 15	Firm Stiff		Adjective (ex: "Silty")	25 - 45				
	0111	sand-silt mixtures	1	- <2.00									
11	SC	CLAYEY SAND	1	- <4.00 - 8.00	16 - 30 31 - 50	Very Stiff Hard							
		sand-clay mixtures	1	3.00 3.00	>50	Very Hard							
	ML	SILT				vory riara			WATER LEVELS				
		non-plastic to medium plasticity	GRAVE	IS SANDS	& NON-C	OHESIVE SIL	TS	WL (I	First Encountered				
	MH	ELASTIC SILT		_0, 0,20 SPT ⁵				- `					
	~	high plasticity				DENSITY		₩L (Completion)				
$\langle \rangle$	CL	LEAN CLAY low to medium plasticity		<5		Very Loose		V WL (Seasonal High W				
	СН	FAT CLAY	1	5 - 10 1 - 30	N /	Loose edium Dense							
	011	high plasticity	1	1 - 30 1 - 50	IVI	Dense		🕎 WL (Stabilized)				
555	OL	ORGANIC SILT or CLAY		>50		Very Dense		- ·					
555		non-plastic to low plasticity											
\mathbb{Z}	ОН	ORGANIC SILT or CLAY				FILL		ОСК					
111		high plasticity	_										
6 56													
36 3		highly organic soils											

¹Classifications and symbols per ASTM D 2488-17 (Visual-Manual Procedure) unless noted otherwise.

²To be consistent with general practice, "POORLY GRADED" has been removed from GP, GP-GM, GP-GC, SP, SP-SM, SP-SC soil types on the boring logs.

³Non-ASTM designations are included in soil descriptions and symbols along with ASTM symbol [Ex: (SM-FILL)].

⁴Typically estimated via pocket penetrometer or Torvane shear test and expressed in tons per square foot (tsf).

⁵Standard Penetration Test (SPT) refers to the number of hammer blows (blow count) of a 140 lb. hammer falling 30 inches on a 2 inch OD split spoon sampler

required to drive the sampler 12 inches (ASTM D 1586). "N-value" is another term for "blow count" and is expressed in blows per foot (bpf). SPT correlations per 7.4.2 Method B and need to be corrected if using an auto hammer.

⁶The water levels are those levels actually measured in the borehole at the times indicated by the symbol. The measurements are relatively reliable when augering, without adding fluids, in granular soils. In clay and cohesive silts, the determination of water levels may require several days for the water level to stabilize. In such cases, additional methods of measurement are generally employed.

⁷Minor deviation from ASTM D 2488-17 Note 14.

⁸Percentages are estimated to the nearest 5% per ASTM D 2488-17.

WATER LEVELS⁶

WL (First Encountered)

WL (Seasonal High Water)

ROCK

FINE

GRAINED

(%)⁸

<5

10 - 25

30 - 45



SUBSURFACE EXPLORATION PROCEDURE: STANDARD PENETRATION TESTING (SPT) ASTM D 1586 Split-Barrel Sampling

Standard Penetration Testing, or **SPT**, is the most frequently used subsurface exploration test performed worldwide. This test provides samples for identification purposes, as well as a measure of penetration resistance, or N-value. The N-Value, or blow counts, when corrected and correlated, can approximate engineering properties of soils used for geotechnical design and engineering purposes.

SPT Procedure:

- Involves driving a hollow tube (split-spoon) into the ground by dropping a 140-lb hammer a height of 30-inches at desired depth
- Recording the number of hammer blows required to drive split-spoon a distance of 12 inches (in 3 or 4 Increments of 6 inches each)
- Auger is advanced* and an additional SPT is performed
- One SPT test is typically performed for every two to five feet
- Obtain two-inch diameter soil sample

*Drilling Methods May Vary— The predominant drilling methods used for SPT are open hole fluid rotary drilling and hollow-stem auger drilling.







 Project No.:
 35-29020-A1

 Boring No.:
 NB87

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Boring Location: See Field Exploration Plan Groundwater Depth: 3.8 ft Time: Drilling Date: 8/10/2 Output Had Had Had B <	Dri Cas 1 Bor 	ll Rig: ll Rod: ing Siz ing Be	<u>AW</u> ze: gun:	J	21	Drill Leng	er: <u>C.]</u> Mud: th of Ca	Super (
Groundwater Depth: 3.8 ft Time: Drilling Date: 8/10/2 O IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	Cas 1 Bor E 9	ing Siz	ze: gun:		21	Leng							
	6 IN.	ring Be	Ĭ	<u>8/10/2</u>	21		Length of Casing:						
ON BITH, FEET ON BITH, FEET MPLE NO DESCRIPTION	R 6 IN.		0			Borir	ng Comj		8/10/21				
S B S	BLOWS PER	N Value	PERCENT ORGANIC MATERIAL	PERCENT PASSING NO. 200 SIEVE	 OPLASTIC LIMIT 0 	+ (%) (%) 0		 Pock Undis Pock Distu Torva Unco 	R STRENGT (ksf) et Penetromete sturbed Sample et Penetromete rbed Sample inne infined Compression	er er ssion			
0 Topsoil 1 LOOSE Light Brown Fine SAND With Shell Fragments (SP)	2 4 6	6											
2 LOOSE Gray Brown Fine SAND With Shell Fragments (SP)	7 4 4 3 3	8											
3 5 VERY LOOSE Gray Fine SAND With Shell Fragments (SP) LOOSE Dark Gray Fine SAND (SP)	2 2 1 4	4											
4	4 4 4 5	8											
5 MEDIUM DENSE Gray Clayey Fine SAND, Few Organic Fines (SC)	6 11 12	17											
6 MEDIUM DENSE Dark Gray Fine SAND (SP)	10 7 7	14											
7 E 20 E MEDIUM DENSE Gray Fine SAND With Shell	4 10 16	26											
8	11 12 18	30											
Boring Terminated @ 25 ft.	-									<u> </u>			



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 Boring No.:
 NB88

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Project	: <u>River</u>	ding Natural Lots - L	Client: <u>HyDry Company, LLC</u> Drill Rig: <u>104A</u> Driller: <u>C. Morgan</u>															
Boring	Location	n:	See Field Exploration	Plan			Dri	l Rod:	AW		Drill Mud: Super Gel-X							
									ze:			Length of Casing:						
Groundwater Depth: <u>4.2 ft</u> Time: <u>Drilling</u> Date: <u>7/28/21</u>									gun:	7/28/								
SAMPLE NO.	O DEPTH, FEET	SAMPLE TYPE	DESCRIPTION				BLOWS PER 6 IN.	N Value	PERCENT ORGANIC MATERIAL	PERCENT PASSING NO. 200 SIEVE		+ 00 (%) (%) (%)		 ○ Pc Ur ○ Pc Dis ○ To ○ Ur 	EAR STREM (ksf) bocket Penetrom disturbed Sampl sturbed Sampl invane nconfined Com iaxial Compres	neter nple neter le		
1			Topsoil LOOSE Brown Fine SA (SP)			s	4 4 5 4	9										
2		-	MEDIUM DENSE Gray Fragments (SP)				6 7 7 8	14										
3	5		VERY LOOSE Brown S			¥ : : : : : : : : : : : : : : : : : : :	5 2 1 3	3										
4			MEDIUM DENSE Gray				3 5 7 6	12										
5	10		MEDIUM DENSE Brov (SP-SC)	vn Fine SAND	With Clay		9 12 16 17	28										
6	15		VERY LOOSE Gray Br With Shell Fragments (S	own Clayey Fi SC)	ine SAND		4 1 2	3										
7	20		MEDIUM DENSE Gray Fragments (SP)	7 Fine SAND V	With Shell		9 5 6	11										
8	25		Boring Terr	ninated @ 25	ft.		10 12 11	23										
Remar	·ks																	



 Project No.:
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 Boring No.:
 NA87

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Project	: <u>River L</u>	Landi	ng Natural Lots - I	_ Client: <u>HyDry Company, LLC</u> _ Drill Rig: <u>104A</u> Driller: <u>C. Morgan</u>												
Boring	Location:	Se	e Field Exploration	Dril	1 Rod:	Flig	4 ht Au	ger	Driller: <u>C. Morgan</u> Drill Mud:							
Ground	Juvotor Do	nthe	2.4.ft Time:	Drilling	Date:	8/10/21	_ Casi	ing Siz ing Be	xe:	<u> 8/10/</u>	- 21]	Length	10/21		
Groundwater Depth: <u>3.4 ft</u> Time: <u>Drilling</u> Date: <u>8/10/21</u>											21			Com	pleted: <u>8/</u> SHEAR S	TRENGTH
SAMPLE NO.	DEPTH,	SAMPLE I YPE	DESCRIPTION	1		0 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	BLOWS PER 6 IN.	N Value	PERCENT ORGANIC MATERIAL	PERCENT PASSING NO. 200 SIEVE		-	+ CONTENT		 ● Pocket Poundisturb ● Pocket Poundisturbed ● Pocket Poundisturbed ● Torvane 	tsf) enetrometer ed Sample enetrometer Sample ed Compression
1 2 3 4 5	0 5 5 10 10 20 20 25	Lig (SF Gra Bro Gra (SC	ay Brown Fine SAND wm Fine SAND (SP ay Brown Clayey Fir) ay Clayey Fine SAN	D (SP) ?) ne SAND Wit	h Wood Pie	ces										
Remar	·ks															



 Project No.:
 35-29020-A1

 Boring No.:
 NA88

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Project: River Landing Natural Lots - Lot 57 Client: HyDry Company, LLC Drill Rig: 104A Driller: C. Morgan																	
Boring	Location	: 5	See Field Explo	ration Plan	Dril	Drill Rod: Flight Auger Drill Mud:							-				
Ground	lwater De	enth	: <u>5 ft</u> Time	e: Drilling	Date:	7/28/21	_ Cas Bor	ing Siz ing Be	ze:	7/28/	21	Length of Casing: Boring Completed: 7/28/21					
SAMPLE NO.	DEPTH, FEET	SAMPLE TYPE	DESCRIPT				BLOWS PER 6 IN.	N Value		PERCENT PASSING NO. 200 SIEVE		(%) + MOISTURE			SHEAR ST (kg Pocket Per Undisturbed Pocket Per Disturbed Torvane Unconfined	TRENGTH of) hetrometer d Sample hetrometer Sample	
1 2 3	5 5 10 10 20 20	I	Dark Gray and Br Gray Clayey Fine	own Fine SAND (S SAND (SC) g Terminated @ 10	5P)												