



November 10, 2021

Mr. Maurice Rudolph HYDRY Company, LLC 4314 Pablo Oaks Court Jacksonville, Florida 32224

> ECS Project No. 35:29020-A1 Client ID: 3524

#### Reference: Preliminary Report of Geotechnical Exploration **River Landing Lot 30** Nocatee, St. Johns County, Florida

Dear Mr. Rudolph:

ECS Florida, LLC (ECS) has completed the requested preliminary geotechnical exploration in general accordance with our Proposal No. 35:17711-GPR dated April 5, 2021. The exploration was performed to explore the general subsurface conditions within the proposed lot area and to provide preliminary recommendations for foundation support.

Additional field testing should be performed to formulate detailed foundation design and site preparation and earthwork construction recommendations prior to final design. Once more detailed information regarding the proposed structure is developed, we should be given the opportunity to review and develop a supplemental design-phase scope of services.

#### **PROJECT INFORMATION**

The general site location is shown on the Site Location Diagram (Figure 1). At the time of our exploration, the site was undeveloped, with ground surface cover consisting of brush and trees. Surface water was not observed near the planned building area at the time of our exploration.

You provided a copy of a site plan for the subject site. This plan indicates the boundary limits for the property and the existing roadways adjacent to the site. However, we note the location of the proposed structure(s) was not available to our office at the time of this report preparation.

The following information explains our assumptions of the planned development.

SUBJECT	DESIGN INFORMATION / ASSUMPTIONS
# of Stories	3 stories above grade
Usage	Residential
Column Loads <sup>(1)</sup>	50 kips
Wall Loads <sup>(1)</sup>	3 kips per linear foot (klf) maximum
Floor Loads <sup>(1)</sup>	150 pounds per square foot (psf) maximum
Fill and Cut Heights	Assumed a maximum of 3 feet of fill and only minor cuts, from existing site grades

(1) If actual structural loads differ from these assumed loads ECS must be contacted immediately in order to revise building foundation recommendations and settlement calculations, as needed.

#### FIELD EXPLORATION

We performed a field exploration on August 25, 2021 and September 9, 2021. The approximate boring locations are indicated on the attached Field Exploration Diagram (Figure 2). Our personnel determined the boring locations using a handheld Global Positioning System (GPS) unit. The boring locations on the referenced Field Exploration Diagram should be considered accurate only to the degree implied by the method of measurement used.

We located and performed two Standard Penetration Test (SPT) borings, drilled to depths of approximately 20 feet below the existing ground surface, in general accordance with the methodology outlined in ASTM D 1586 and two auger borings, drilled to depths of approximately 10 feet below the existing ground surface in general accordance with the methodology outlined in ASTM D 1452 to explore the subsurface conditions within the lot area. Soil samples recovered during performance of the borings were visually classified in the field and representative portions of the samples were transported to our laboratory for further evaluation. Our exploration procedures are explained in greater detail in Appendix B including the insert titled Subsurface Exploration Procedures.

#### VISUAL CLASSIFICATION

Each sample was visually classified on the basis of texture and plasticity in accordance with ASTM D2488 Standard Practice for Description and Identification of Soils (Visual-Manual Procedures) and including USCS classification symbols, and ASTM D2487 Standard Practice for Classification for Engineering Purposes (Unified Soil Classification System (USCS)). After classification, the samples were grouped in the major zones noted on the boring logs in Appendix B. The group symbols for each soil type are indicated in parentheses along with the soil descriptions. The stratification lines between strata on the logs are approximate; in situ, the transitions may be gradual.

#### **GENERAL SUBSURFACE CONDITIONS**

A graphical presentation of the generalized subsurface conditions is presented on Figure 3. It should be understood that the soil conditions will vary between the boring locations and in areas of the site not explored during our visit. The following table summarizes the soil conditions encountered.

Typical De	epth (ft)	Stratum	Description
From	То		
Existing Ground Surface	0.5 – 1	N/A	Topsoil
0.5 – 1	1 ½ - 2 ½	I	Very Loose to Loose FINE SAND (SP), With Shell Fragments, Moist to Wet
1 ½ - 2 ½	3-4	П	Organic CLAY (OL), Moist to Wet
3-4	8	111	Loose to Medium Dense, FINE SAND (SP), FINE SAND WITH CLAY (SP- SC), and CLAYEY FINE SAND (SC), Moist to Wet
8	20	IV	Medium Dense FINE SAND (SP) and FINE SAND WITH SILT (SP-SM), Wet

A graphical presentation of the subsurface conditions is shown on the Generalized Subsurface Soil Profiles in Appendix A.

Groundwater was encountered at each boring location and recorded at the time of drilling at depths varying from 3 feet to 5.4 feet below the existing ground surface. We note that groundwater levels will fluctuate due to seasonal climatic variations, surface water runoff patterns, construction operations, and other interrelated factors. The groundwater depth at each boring location is noted on the Generalized Subsurface Profiles and on the Log of Boring records.

#### PRELIMINARY DESIGN RECOMMENDATIONS

Our geotechnical engineering evaluation of the site and subsurface conditions at the property, with respect to the planned construction and our recommendations for earthwork and foundation support, are based on (1) our site observations, (2) the field and laboratory test data obtained, (3) our understanding of the project information and structural conditions as presented in this report, and (4) our experience with similar soil and loading conditions.

Additional field testing should be performed to formulate detailed foundation design and site preparation and earthwork construction recommendations prior to final design. Also, the discovery of any site or subsurface conditions during construction that deviate from the data obtained during this geotechnical exploration should also be reported to us for our evaluation.

Based on the above preliminary evaluation of the site and subsurface conditions at the borings with respect to the anticipated construction, it appears the proposed structure can be constructed on a conventional shallow foundation system provided the organic-containing soils are removed from below the structure.

#### **Conventional Shallow Foundation Support – (Option 1)**

The planned residential structure can be supported by a conventional shallow foundation system ("spread footings") provided the site is properly prepared. As described previously, two of the borings encountered organic containing material at depths of 2 ½ feet to 3 feet and to 1 ½ feet to 4 feet below the existing ground surface. While the overlying sands appear suitable for structural fill, we do not recommend that this organic-containing material be left in-place below the planned structure. We therefore recommend that this material be removed from within and 5-feet beyond planned structural areas. The overlying sands can be replaced in the resulting excavation and compacted in lifts. We recommend additional test pits be

performed prior to or concurrent with over-excavation to better delineate the horizontal extents of materials requiring removal. Subsequent to these site preparation activities, we expect that shallow spread foundations can be designed for an allowable bearing capacity of 2,500 psf.

#### **Deep Foundation Support – (Option 2)**

The organic-containing soils can be left in-place if the proposed structure (including the floor slabs) is supported by deep foundations. There are several types of deep foundations; however, based on our experience with similar projects and soil conditions, Auger Cast In-Place (ACIP) piles are applicable. ACIP piles are constructed by drilling into the subsurface material with a continuous flight auger which is pulled upward (after achieving the required length) while cement grout is pumped under pressure through the auger. Based on our experience with similar soil conditions, we expect that a 14-inch ACIP bearing 20-feet below the existing grades may develop an axial capacity on the order of 15 tons.

#### **REPORT LIMITATIONS**

Our geotechnical exploration has been performed, our findings obtained, and our recommendations prepared, in accordance with generally accepted geotechnical engineering principles and practices. ECS is not responsible for any independent conclusions, interpretation, opinions, or recommendations made by others based on the data contained in this report. Additional field testing should be performed to formulate detailed foundation design and site preparation and earthwork construction recommendations prior to final design.

Respectfully Submitted **ECS FLORIDA, LLC** 

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#### APPENDICES

#### **Appendix A – Drawings & Reports**

- Figure 1 Site Location Diagram
- Figure 2 Field Exploration Diagram
- Figure 3 Generalized Subsurface Profiles

#### **Appendix B – Field Operations**

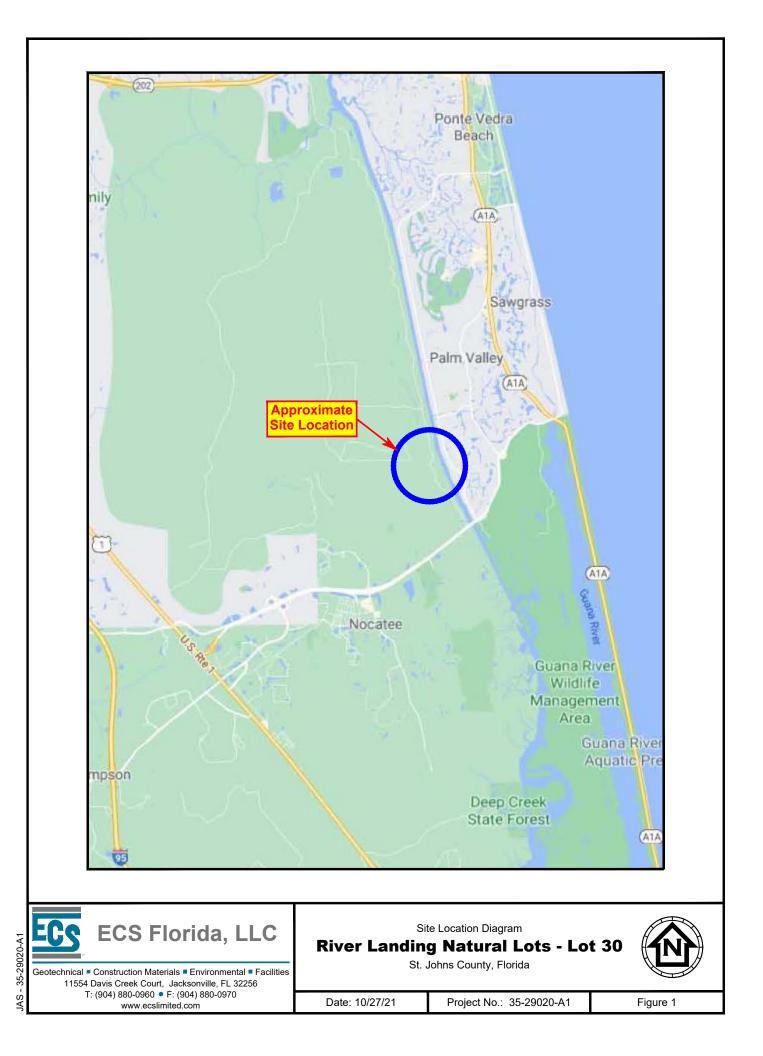
- Reference Notes for Boring Logs
- Subsurface Exploration Procedure: Standard Penetration Testing (SPT)
- Boring Logs

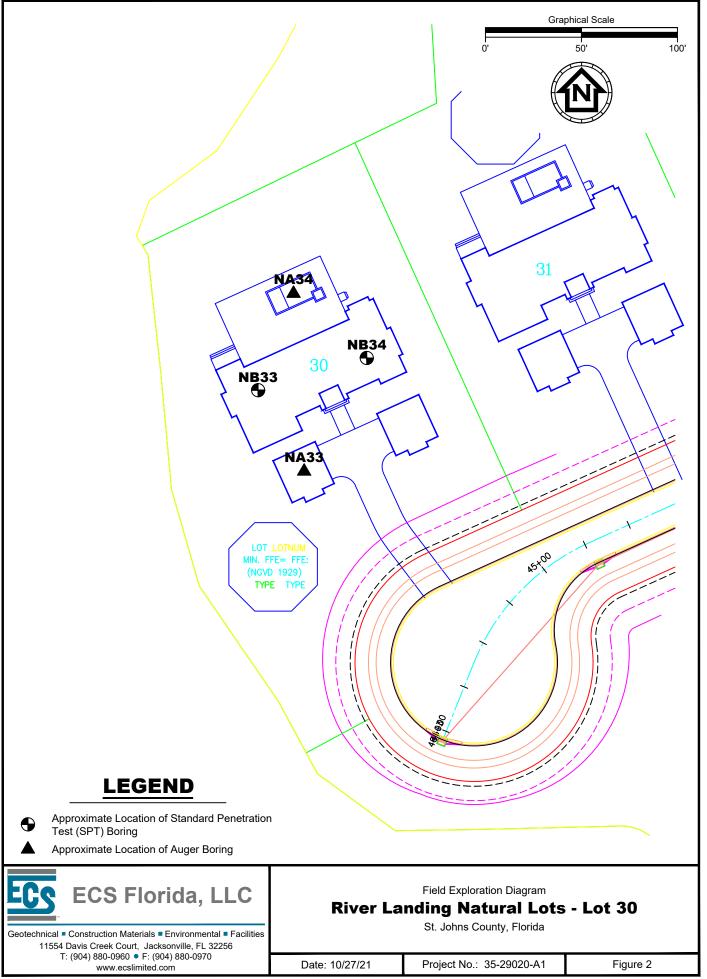
### **APPENDIX A – Drawings & Reports**

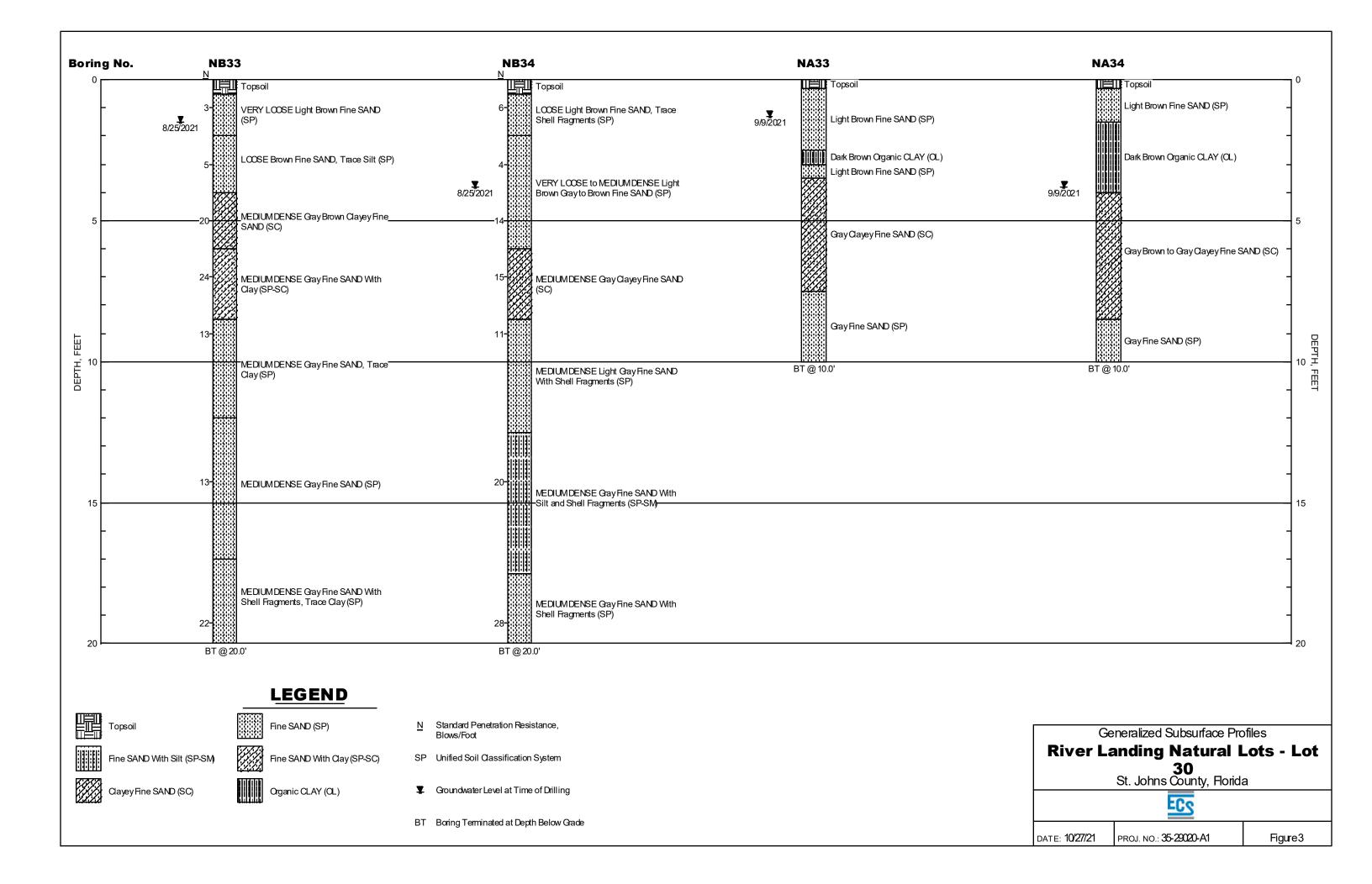
Figure 1 - Site Location Diagram

Figure 2 - Field Exploration Diagram

Figure 3 - Generalized Subsurface Profiles







## **APPENDIX B – Field Operations**

Reference Notes for Boring Logs Subsurface Exploration Procedure: Standard Penetration Testing (SPT) Boring Logs



# **REFERENCE NOTES FOR BORING LOGS**

	1						
ACD	HALT	SS	Split Spoo	n Sampler		PM	
ASPI		ST	Shelby Tu	be Sample	er	RD	
CON	ODETE	WS	Wash Sam	nple		RC	
CON	GREIE	BS	Bulk Samp	ole of Cutti	ngs	REC	
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		Sand:	Coarse	2.0	0 mm to 4.7	5 mm (N	ło
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	-		Fine	0.0	74 mm to 0.4	425 mm	1)
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66	-				OLATO		
GC	-			SDT2	CONSISTE		
SW	-						
300							
SP		1			-	JI	
01		1					
SM							
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-	sand-clay mixtures	1				1	
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	non-plastic to medium plasticity	OD AV					
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	high plasticity		SPT°		DENSITY		
CL	LEAN CLAY		<5		Very Loose		
	low to medium plasticity		5 - 10		Loose	1	
СН	FAT CLAY	1	1 - 30	М	ledium Dens	e	
	high plasticity	3	31 - 50		Dense		
OL	ORGANIC SILT or CLAY		>50		Very Dense		
он	ORGANIC SILT or CLAY				EII		P/
	high plasticity						n.c
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<sup>1</sup>Classifications and symbols per ASTM D 2488-17 (Visual-Manual Procedure) unless noted otherwise.

<sup>2</sup>To be consistent with general practice, "POORLY GRADED" has been removed from GP, GP-GM, GP-GC, SP, SP-SM, SP-SC soil types on the boring logs.

<sup>3</sup>Non-ASTM designations are included in soil descriptions and symbols along with ASTM symbol [Ex: (SM-FILL)].

<sup>4</sup>Typically estimated via pocket penetrometer or Torvane shear test and expressed in tons per square foot (tsf).

<sup>5</sup>Standard Penetration Test (SPT) refers to the number of hammer blows (blow count) of a 140 lb. hammer falling 30 inches on a 2 inch OD split spoon sampler

required to drive the sampler 12 inches (ASTM D 1586). "N-value" is another term for "blow count" and is expressed in blows per foot (bpf). SPT correlations per 7.4.2 Method B and need to be corrected if using an auto hammer.

<sup>6</sup>The water levels are those levels actually measured in the borehole at the times indicated by the symbol. The measurements are relatively reliable when augering, without adding fluids, in granular soils. In clay and cohesive silts, the determination of water levels may require several days for the water level to stabilize. In such cases, additional methods of measurement are generally employed.

<sup>7</sup>Minor deviation from ASTM D 2488-17 Note 14.

<sup>8</sup>Percentages are estimated to the nearest 5% per ASTM D 2488-17.

essuremeter Test ck Bit Drilling ck Core, NX, BX, AX ck Sample Recovery % ck Quality Designation %

	PARTICLE SIZE IDENTIFICATION										
DESIGNATI	ON	PARTICLE SIZES									
Boulders		12 inches (300 mm) or larger									
Cobbles		3 inches to 12 inches (75 mm to 300 mm)									
Gravel:	Coarse	3/4 inch to 3 inches (19 mm to 75 mm)									
	Fine	4.75 mm to 19 mm (No. 4 sieve to <sup>3</sup> / <sub>4</sub> inch)									
Sand:	Coarse	2.00 mm to 4.75 mm (No. 10 to No. 4 sieve)									
	Medium	0.425 mm to 2.00 mm (No. 40 to No. 10 sieve)									
	Fine	0.074 mm to 0.425 mm (No. 200 to No. 40 sieve)									
Silt & Cla	y ("Fines")	<0.074 mm (smaller than a No. 200 sieve)									

RELATIVE AMOUNT <sup>7</sup>	COARSE GRAINED (%) <sup>8</sup>	FINE GRAINED (%) <sup>8</sup>				
Trace	<u>&lt;</u> 5	<5				
With	10 - 20	10 - 25				
Adjective (ex: "Silty")	25 - 45	30 - 45				

WATER	LEVELS <sup>6</sup>

t Encountered)
t Encountered)

- WL (Completion)
- WL (Seasonal High Water)
- WL (Stabilized)

FILL AND ROCK											
FILL		PROBABLE FILL	ROCK								



## SUBSURFACE EXPLORATION PROCEDURE: STANDARD PENETRATION TESTING (SPT) ASTM D 1586 Split-Barrel Sampling

Standard Penetration Testing, or **SPT**, is the most frequently used subsurface exploration test performed worldwide. This test provides samples for identification purposes, as well as a measure of penetration resistance, or N-value. The N-Value, or blow counts, when corrected and correlated, can approximate engineering properties of soils used for geotechnical design and engineering purposes.

## **SPT Procedure:**

- Involves driving a hollow tube (split-spoon) into the ground by dropping a 140-lb hammer a height of 30-inches at desired depth
- Recording the number of hammer blows required to drive split-spoon a distance of 12 inches (in 3 or 4 Increments of 6 inches each)
- Auger is advanced\* and an additional SPT is performed
- One SPT test is typically performed for every two to five feet
- Obtain two-inch diameter soil sample

\*Drilling Methods May Vary— The predominant drilling methods used for SPT are open hole fluid rotary drilling and hollow-stem auger drilling.







 Project No.:
 35-29020-A1

 Boring No.:
 NB33

 Sheet
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 of
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Project	: <u>River</u>	Lar	nding Natural Lots - L	ot 30				ent: <u>H</u>			any, I			Manaan		
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							Cas	ing Siz	ze:			Lengt	h of Ca	sing:		
Ground	lwater D	epth	n: <u>1.5 ft</u> Time:	Drilling	_ Date:	8/25/21	_ Bor	oring Begun:		8/25/2	21	Borin	8/25/21			
SAMPLE NO.	O DEPTH, FEET	SAMPLE TYPE	DESCRIPTION				BLOWS PER 6 IN.	N Value	PERCENT ORGANIC MATERIAL	PERCENT PASSING NO. 200 SIEVE		+ WOISTURE + 0012TURE + 0012TURE	- 6 <b>CLIQUID LIMIT</b>	<ul> <li>Pock Undi</li> <li>Pock Distu</li> <li>Torva</li> <li>Unco</li> </ul>	AR STRENG (ksf) tet Penetrome sturbed Sample ane onfined Comp ial Compressi	eter ble eter ression
1			Topsoil VERY LOOSE Light Bi LOOSE Brown Fine SA			<b>T</b>	1 1 2 2 1	3								
2			MEDIUM DENSE Gray		. ,	ND ////	2 3 4 6	5								
3	5		(SC) MEDIUM DENSE Gray	_	-		8 12 9 9	20								
4			(SP-SC)		-		11 13 16 6	24								
5	10		MEDIUM DENSE Gray (SP)	7 Fine SAND, 7	Trace Clay	r	5 8 8	13								
6	- 15 -		MEDIUM DENSE Gray	Fine SAND (	SP)		5 5 8	13								
			MEDIUM DENSE Gray Fragments, Trace Clay (	V Fine SAND V (SP)	With Shell											
7	20		Boring Terr	ninated @ 20	ft.		9 11 11	22								
	25															
Remar																



 Project No.:
 35-29020-A1

 Boring No.:
 NB34

 Sheet
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 of
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Project	: <u>River</u>	Lar	nding Natural Lots - I	.ot 30				ent: <u>H</u> ll Rig:			any, LI			Morran				
Boring	Location	n:	See Field Exploration	ı Plan			Dri	l Rod:	AW			Driller: <u>C. Morgan</u> Drill Mud: <u>Super Gel-X</u>						
			-		D	0/25/21	_ Cas	ing Siz	ze: _	0/05/	0.1	Lengt	h of Ca	ising:	0.5./0.1			
Ground	iwater D	eptr	n: <u>3.8 ft</u> Time:	Drilling	_ Date:	8/25/21	_ Bor	ring Begun:		8/25/	21	Borin	g Com	npleted: 8/25/21 SHEAR STRENGTH				
SAMPLE NO.	o DEPTH, FEET	SAMPLE TYPE	DESCRIPTION			6	BLOWS PER 6 IN.	N Value	PERCENT ORGANIC MATERIAL	PERCENT PASSING NO. 200 SIEVE		+ MOISTURE + CONTENT		(I ● Pocket P Undisturk ● Pocket P Disturbed ▼ Torvane ● Unconfine	enetrometer bed Sample enetrometer i Sample ed Compression ompression			
1			Topsoil LOOSE Light Brown Fr Fragments (SP)				2 3 3 3	6										
2			VERY LOOSE Light B	·	x	SP)	4 3 1 2	4										
3	5		MEDIUM DENSE Brow				4 5 9 4	14										
4			MEDIUM DENSE Gray	<sup>7</sup> Clayey Fine S	SAND (SC		4 6 9 12 4	15										
5	10		MEDIUM DENSE Ligh Shell Fragments (SP)	t Gray Fine SA	ND With		4 5 6 9	11										
6	15		MEDIUM DENSE Gra Shell Fragments (SP-SN	7 Fine SAND W (1)	Vith Silt ar	nd	5 8 12	20										
7	20		MEDIUM DENSE Gray Fragments (SP) Boring Terr	y Fine SAND W			13 13 15	28										
	25		boring ren	accu ( <u>w</u> 20 1														
Rema	rks																	



 Project No.:
 35-29020-A1

 Boring No.:
 NA33

 Sheet
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Project	River	Lan	ding Natural Lots - L	Client: <u>HyDry Company, LLC</u> Drill Rig: <u>101A</u> Driller: <u>M. Foster</u>												
Boring	Location	: :	See Field Exploration	Plan			_ Dril	l Rod:	Flig	A ht Au	ger	Drill Mud:				
					D (	0/0/21	Casi	ng Siz	e:		-	L	ength o	of Cas	sing:	21
Ground	water De	epth	: <u>1.3 ft</u> Time:	Drilling	_ Date: _	9/9/21	Boring Begun: <u>9/9/21</u>					Boring Completed: 9/9/21 SHEAR STRENGTH				
SAMPLE NO.	DEPTH,	SAMPLE TYPE	DESCRIPTION			6.1.223	BLOWS PER 6 IN.	N Value	PERCENT ORGANIC MATERIAL	PERCENT PASSING NO. 200 SIEVE		- 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0			(k ● Pocket Pe Undisturbe ● Pocket Pe Disturbed ▼ Torvane	sf) enetrometer ed Sample netrometer Sample d Compression
1 2 3 4 5	0 5 10 10 20 20	I	Topsoil Light Brown Fine SANI Dark Brown Organic CI Light Brown Fine SANI Gray Clayey Fine SANI Gray Fine SAND (SP) Boring Terr	LAY (OL)	  t.											
Remar							I						, '			



 Project No.:
 35-29020-A1

 Boring No.:
 NA34

 Sheet
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 of
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Project	: <u>River l</u>	Landing Natural Lots -	Lot 30	Client: <u>HyDry Company, LLC</u> Drill Rig: <u>104A</u> Driller: <u>C. Morgan</u>								
Boring	Location	: See Field Exploration	on Plan		Dril	l Rod:	Flight	Auger	Ľ	Drill Mud:	-	
Ground	lwater De	epth: <u>3.8 ft</u> Time:	Drilling Date:	9/9/21	_ Casi Bori	ng Siz ng Beg	e: gun: <u>9/</u>	9/21	L B	ength of C Boring Com	asing: pleted: _ <u>9/9</u>	0/21
SAMPLE NO.	FEET				BLOWS PER 6 IN.		NT ORGANIC ATERIAL ENT PASSING		WOISTURE +	CONTENT CONTENT	SHEAR S         (k         ● Pocket Pe         ● Disturbed         ▼ Torvane	TRENGTH sf) netrometer dd Sample netrometer Sample d Compression
1 2 3 4 5	0 5 5 10 10 20 20	Topsoil Light Brown Fine SAI Dark Brown Organic Gray Brown Clayey F Gray Clayey Fine SAN Gray Fine SAND (SP) Boring Te	CLAY (OL) ine SAND (SC) ND (SC)									
Remar												